

DESCRIPTION

VALVE TRAIN FOR INTERNAL COMBUSTION ENGINE

5 Technical Field

The present invention relates to a valve train for an internal combustion engine, and more particularly to a valve train which can change the valve operating properties including opening and closing timings and 10 maximum lift amount of an engine valve made up of at least one of an inlet valve and an exhaust valve.

Background Art

As a valve train for an internal combustion engine 15 in which the valve operating properties of an engine valve are changed in accordance with an oscillating position of an oscillating member which supports a transmission mechanism which transmits the valve drive force of a valve operating cam to the engine valve, there 20 is a valve train disclosed, for example, in Japanese Patent Unexamined Publication No. JP-A-7-91217. The valve train disclosed in the JP-A-7-91217 includes a drive shaft which is driven to rotate by an internal combustion engine, a camshaft which is disposed rotatably 25 on an outer circumference of the drive shaft and which is

provided rotatably on a cylinder head, a cam formed on
the camshaft, a disk housing adapted to oscillate in a
radial direction relative to the drive shaft about a
pivot pin acting as a fulcrum, an annular disk which is
5 rotatably supported on an inner circumferential surface
of the disk housing, a drive mechanism for oscillating
the disk housing and a rocker arm which is pivot
supported on a rocker shaft which is supported, in turn,
on the disk housing at one end portion thereof and which
10 abuts with the cam and an inlet valve.

Then, when the disk housing is caused to oscillate
by the drive mechanism, the center of the annular disk
becomes eccentric to the axial center of the drive shaft,
so that the rotational phase difference and rotational
15 angular velocity ratio of the cam and the drive shaft
change, whereby the operation angle of the inlet valve is
changed. At the same time, the pivot fulcrum position of
the rocker arm is changed through the displacement of the
rocker shaft which oscillates together with the disk
20 housing, and the other end portion of the rocker arm
shifts over an upper surface of a valve lifter along a
diametrical direction thereof, whereby a rocker ratio
relative to the inlet valve is changed so that the valve
lift amount is changed.

25 In the related art disclosed in the JP-A-7-91217,

since a cam abutment position between the cam and the rocker arm is situated substantially on a straight line which passes a rotational center line of the cam and an oscillating center line of the disk housing on a plane 5 which intersects with the oscillating center line at right angles, a moment acting on the disk housing based on a valve drive force acting at the cam abutment position is reduced when the rocker arm is in abutment with a lobe portion of the cam, whereby the drive force 10 of the drive mechanism which is necessary to oscillate the disk housing is reduced. However, since the rocker arm abuts with both the cam and the inlet valve, the related art has the following drawbacks.

Namely, when attempting to maintain the closed state 15 of the inlet valve with the rocker arm being allowed to abut with a base circle of the cam, since the cam abutment position cannot be shifted largely on the base circle of the cam, the oscillating amount of the pivot support position of the rocker arm by virtue of 20 oscillation of the disk housing is limited to a relatively small value, and this disables a large change in rotational phase difference, rotational angular velocity ratio and rocker ratio, thereby making it difficult to increase the control range of the opening 25 and closing timings and maximum lift amount of the inlet

valve. In addition, since the pivot fulcrum position and pivot pin position are determined unconditionally from the positional relation between the cam and the inlet valve, the degree in freedom in arrangement of the rocker arm and the pivot pin is limited, and with, for example, 5 an internal combustion engine having a relatively compact cylinder head, the interference of the valve train with peripheral members of the engine which are disposed therearound cannot be avoided, and it becomes difficult 10 to dispose the valve train of the related art within the limited space, resulting in the possible occurrence of a risk that the related art valve train cannot be adopted for the aforesaid internal combustion engine. In 15 addition, when attempting to have a specific positional relation between the abutment position of the rocker arm with the inlet valve and the oscillating center line, in addition to the positional relation among the cam abutment position, the rotational center line and the oscillating center line, the degree of freedom is reduced 20 further.

Disclosure of the Invention

The present invention was made in view of the situations. An object of the present invention is to 25 provide a valve train for an internal combustion engine

including a transmission mechanism for transmitting a valve drive force of a valve operating cam to an engine valve and in which valve operating properties are changed in accordance with an oscillating position of a holder of

5 the transmission mechanism, wherein a drive mechanism for oscillating the holder can be made compact in size by reducing the drive force of the drive mechanism, and wherein the control range of the valve operating properties can be set large and the degree of freedom in

10 arrangement of the transmission mechanism can be increased. Also, another object of the present invention is to provide a valve train which can suppress the progress in wear of a valve abutment portion or the engine valve due to the oscillation of the holder.

15 Furthermore, the other object of the present invention is to reduce further the drive force of the drive mechanism.

According to a first aspect of the present invention, there is provided a valve train for an internal combustion engine, comprising:

20 a valve operating cam rotating around a rotational center line in synchronism with a rotation of an engine; an engine valve including at least one of an inlet valve and an exhaust valve;

a transmission mechanism for transmitting a valve drive force of the valve operating cam to the engine

valve so as to operate the engine valve in opening and closing states, the transmission mechanism including:

5 a primary oscillating member having an abutment portion which abuts with the valve operating cam, and oscillating about a primary oscillating center line by the valve operating cam;

10 a secondary oscillating member having a valve abutment portion which abuts with the engine valve, transmitting the valve drive force via the primary oscillating member to the engine valve, and oscillating about a secondary oscillating center line;

15 a holder supporting the primary and secondary oscillating members in an oscillatory fashion so that the primary and secondary oscillating center lines rotate together therewith, and oscillating about a holder oscillating center line which differs from the rotational center line of the valve operating cam;

20 a drive mechanism for driving the holder so as to control valve properties including opening and closing timings and maximum lift amount of the engine valve in accordance with an oscillating position of the holder;

25 wherein as the oscillating position of the holder approaches a predetermined position where the maximum lift amount of the valve operating property becomes maximum is obtained, a cam abutment position where a cam

lobe portion of the valve operating cam and the cam abutment portion abut with each other approaches a specific straight line which passes through the holder oscillating center line and the rotational center line.

5 According to the construction, since the line of action of the valve drive force is situated on the specific straight line when the cam abutment position lies on the specific straight line, the moment becomes zero which is generated around the holder oscillating center line to act on the holder based on the valve drive force applied via the primary oscillating member. From this fact, while the valve drive force is increased because the maximum lift amount is increased as the holder approaches the oscillating position where the 10 valve property is obtained where the maximum lift amount of the engine valve becomes maximum, the moment acting on the holder can be reduced by the approach of the cam abutment position on the cam lobe portion to the specific straight line, whereby the drive force of the drive mechanism which oscillates the holder against the moment can be reduced. In addition, the abutment state between the valve operating cam and the engine valve can be set by the separate oscillating member due to the primary and secondary oscillating members abutting with the valve 15 operating cam and the engine valve, respectively, and the 20 25

primary and secondary oscillating center lines oscillate together with the holder. Consequently, even in the event that the shift amount of one of the primary and secondary oscillating members is increased by virtue of
5 the oscillation of the holder in order to set the control range of the valve operating properties large, when compared with a case while one of the primary and secondary oscillating center lines shifts, the other does not, the relative shift amount of the primary and
10 secondary oscillating members can be suppressed to a small level.

According to a second aspect of the present invention as set forth in the first aspect of the present invention, it is preferable that the valve abutment portion having a valve abutment surface which abuts with
15 the engine valve is provided at a position which intersects with the holder oscillating center line.

According to the construction, since the valve abutment surface resides close to the holder oscillating center line, even in the event that the valve abutment position which is the abutment position of the valve abutment surface with the engine valve shifts due to the oscillation of the secondary oscillating center line which is triggered by the oscillation of the holder, the
25 resulting shift amount is reduced, thereby making it

possible to reduce the size of the valve abutment portion.

According to a third aspect of the present invention as set forth in the first aspect of the present 5 invention, it is more preferable that the valve abutment portion abuts with a valve shaft of the engine valve,

the holder oscillating center line is disposed on an extension of the valve shaft which extends along an axis of the valve shaft, and

10 when the cam abutment position is situated at an apex of the cam lobe portion, the cam abutment position is situated on the specific straight line.

According to the construction, since the distance between the holder oscillating center line disposed on 15 the extension of the valve shaft and the line of action of the reaction force from the engine valve is maintained small within the range of the valve shaft, a moment acting on the holder based on the reaction force of the engine valve can be reduced. In addition, when a maximum 20 valve operating force acts at a specific oscillating position of the holder, since the moment acting on the holder based on the valve drive force becomes zero, the drive force of the drive mechanism which oscillates the holder against the moment can be reduced.

25 According to a fourth aspect of the present

invention as set forth in the first aspect of the present invention, it is further preferable that the valve abutment portion abuts with a valve shaft of the engine valve,

5 the holder oscillating center line is disposed on an extension of the valve shaft which extends along an axis of the valve shaft, and

10 the cam abutment portion is disposed such that the cam abutment position is capable of being situated on the specific straight line which passes through the holder oscillating center line and the rotational center line.

According to the construction, since the distance between the holder oscillating center line disposed on the extension of the valve shaft and the line of action of the reaction force from the engine valve is maintained small within the range of the valve shaft, a moment acting on the holder based on the reaction force of the engine valve can be reduced. In addition, in the state where the cam abutment position on the cam lobe portion resides on the specific straight line or in the vicinity thereof, the moment acting on the holder based on the valve drive force can be reduced, and therefore, the drive force of the drive mechanism which oscillates the holder against the moment can be reduced.

According to the invention set forth in the first aspect, the following advantages are provided. Namely, since the drive force of the drive mechanism for oscillating the holder can be reduced, the drive mechanism is made compact in size. Since the abutment state of the valve operating cam with the engine valve can be set by the separate oscillating member, the degree of freedom in arrangement of the transmission mechanism, so that the scope of application of the invention can be expanded. In addition, since the relative shift amount of the primary and secondary oscillating members can be suppressed to a small level, the control range of the valve operating properties can be set large.

According to the invention set forth in the second aspect, in addition to the advantages provided the first aspect referred to therein, the following advantages are provided. Namely, since the shift amount is small even in the event that the valve abutment position is caused to shift due to the oscillation of the holder, the progress in wear of the valve abutment surface attributed to the oscillation of the holder is suppressed. In addition, since the valve abutment portion can be made small in size, the secondary oscillating member is miniaturized.

According to the invention set forth in the third

aspect, in addition to the advantages provided the second aspect referred to therein, the following advantages are provided. Namely, since the moment acting on the holder based on the reaction force of the engine valve can be 5 reduced, in this respect, too, the invention can contribute to the reduction in drive force of the drive mechanism. In addition, since the moment acting on the holder based on a maximum valve drive force at a specific oscillating position becomes zero, the drive force of the 10 drive mechanism can be reduced further, thereby making the drive mechanism compact.

According to the invention set forth in the fourth aspect, in addition to the advantages provided the third aspect referred to therein, the following advantages are 15 provided. Namely, since the moment acting on the holder based on the reaction force of the engine valve can be reduced, in this respect, too, the invention can contribute to the reduction in drive force of the drive mechanism. In addition, since the moment acting on the 20 holder based on the valve drive force becomes zero, the drive force of the drive mechanism can be reduced further, thereby making the drive mechanism compact.

Brief Description of the Drawing

25 Fig. 1 is a sectional view of a main part of an internal

combustion engine having a valve train of the invention,
which shows a first embodiment of the invention.

Fig. 2 is an enlarged view of the main part in Fig. 1,
which is a sectional view taken along the line indicated
5 by arrows IIa-IIa and as viewed in a direction indicated
by the same arrows in Fig. 3 as to a cylinder head, and
which is a sectional view taken along the line indicated
by arrows IIb-IIb and as viewed in a direction indicated
by the same arrows in Fig. 3 as to a transmission
10 mechanism.

Fig. 3 is a view of the valve train with a cylinder head
cover of the internal combustion engine being removed, as
viewed in a direction indicated by an arrow III in Fig.
1.

15 Fig. 4 is a sectional view taken along the line indicated
by arrows IV-IV and as viewed in a direction indicated by
the same arrows in Fig. 3.

Fig. 5 is a graph showing valve operating properties of
the valve train shown in Fig. 1.

20 Fig. 6 is a drawing explaining the operation of an inlet
operation mechanism when a maximum valve operating
property of the valve train shown in Fig. 1 is obtained.

Fig. 7 is a drawing explaining the operation of the inlet
operation mechanism when a minimum valve operating
25 property of the valve train shown in Fig. 1 is obtained.

Fig. 8 is a drawing explaining the operation of the inlet operation mechanism when an intermediate valve operating property of the valve train shown in Fig. 1 is obtained.
Fig. 9 is a drawing showing a second embodiment of the
5 invention, which corresponds to Fig. 6.

Best Mode For Carrying Out the Invention

Embodiments of the invention will be described below by reference to Figs. 1 to 9.

10 Figs. 1 to 8 are drawings which describe a first embodiment of the invention. Referring to Fig. 1, an internal combustion engine E provided with a valve train of the invention is an overhead camshaft, water-cooled, in-line four-cylinder, four-stroke internal combustion engine, and is installed transversely in a vehicle in such a manner that a crankshaft thereof extends in a transverse direction of the vehicle. The internal combustion engine E includes a cylinder block 2 in which four cylinders 1 are formed integrally, a cylinder head 3 connected to an upper end portion of the cylinder block 2 and a cylinder head cover 4 connected to an upper end portion of the cylinder head 3, the cylinder block 2, the cylinder head 3 and the cylinder head cover 4 making up 15 an engine main body of the internal combustion engine E.
20
25 Note that in this specification, it is understood

that a vertical direction denotes a direction which coincides with a cylinder axis direction A1 of the cylinder 1 and that upward denotes a direction in which the cylinder head 3 is disposed relative to the cylinders 5 1 in the cylinder axis direction A1. In addition, a sectional shape means a sectional shape in a plane (hereinafter, simply referred to as an orthogonal plane) which intersects at right angles with a holder oscillating center line L3, a primary oscillating center 10 line L4, a secondary oscillating center line L5 or a rotational center line L2, all of which will be described later on. Then, this orthogonal plane also constitutes an oscillating plane which is a plane parallel to an oscillating direction of a holder 30, a primary rocker 15 arm 50 or a secondary rocker arm 60, all of which will be described later on.

A cylinder bore is formed in each cylinder 1 in which a piston 5 connected to the crankshaft by a connecting rod 6 fits in such a manner as to reciprocate 20 freely therein. In the cylinder head 3, a combustion chamber 7 is formed in a surface which faces the cylinder bores in the cylinder axis direction A1 in such a manner as to correspond to each cylinder 1, respectively, and an inlet port 8 having a pair inlet openings and an exhaust 25 port 9 having a pair of exhaust openings are also formed

in the cylinder head 3 in such a manner as to open to
each combustion chamber 7. A spark plug 10 is installed
in the cylinder head 3 in such a manner as to be inserted
into an insertion hole formed in the cylinder 3 on an
5 exhaust side thereof together with an ignition coil 11
connected to the spark plug 10.

Here, the inlet side of the internal combustion
engine E means a side where an inlet valve 14 or an
entrance 8a to the inlet port 8 is disposed relative to a
10 reference plane H1 which includes cylinder axes L1 and
which is parallel to a rotational center line L2 of an
inlet cam 21 and an exhaust cam 22 which also constitutes
a rotational center line L2 of a camshaft 20, and the
exhaust side of the internal combustion engine E means a
15 side where an exhaust valve 15 or an exit 9a from the
exhaust port 9 is disposed. Then, the inlet side is one
of one side and the other side relative to the reference
plane H1, whereas the exhaust side is the other of the
one side and the other side.

20 In the cylinder head 3, a pair of inlet valves 14
functioning as primary engine valves and a pair of
exhaust valves 15 functioning as secondary engine valves
are provided for each cylinder 1, the inlet valves 14 and
the exhaust valves 15 each being made up of a poppet
25 valve which is supported in a valve guide 12 in such a

manner as to reciprocate therein and is biased in a normally closed direction. The pair of inlet valves 14 and the pair of exhaust valves 15 which belong to each cylinder 1 are operated to be opened and closed by a 5 valve train V so as to open and close the pair of inlet openings and the pair of exhaust openings, respectively. The valve train V, excluding an electric motor 28 for driving a drive shaft 29, which will be described later on, is disposed within a valve chamber 16 defined by the 10 cylinder head 3 and the cylinder head cover 4.

The internal combustion engine E includes further inlet system 17 and an exhaust system 18. The inlet system 17, which includes an air cleaner, a throttle valve and an inlet manifold 17a for induction of air for 15 combustion into the inlet port 8, is mounted on a side on the inlet side of the cylinder head 3 to which the openings 8a of each port 8 are made to open, whereas the exhaust system 18, which includes an exhaust manifold 18a for guiding exhaust gases flowing thereinto from the 20 combustion chambers 7 via the exhaust ports 9 to the outside, is mounted on a side on the exhaust side of the cylinder head 3 to which the openings 9a of each exhaust port 9 are made to open. In addition, a fuel injection valve 19, which is a fuel supply system for supplying 25 fuel for intake air, is installed in the cylinder head 3

in such a manner as to be inserted into an insertion hole provided on the inlet side of the cylinder head 3 so as to face the inlet port 8 of each cylinder 1.

Then, air drawn in through the inlet system 17 is

- 5 drawn further into the combustion chamber 7 from the inlet port 8 via the inlet valves 14 which are opened in an induction stroke where the piston 5 descends and is compressed in a compression stroke where the piston 5 ascends in a state in which the air is mixed with fuel.
- 10 The air/fuel mixture is ignited by the spark plug 10 in a final stage of the compression stroke for combustion, and the piston 5, which is driven by virtue of the pressure of combustion gases in a power stroke where the piston descends, drives and rotates the crankshaft via the connecting rod 6. Combustion gases are discharged from the combustion chamber 7 into the exhaust port 9 as exhaust gases via the exhaust valves 15 which are opened in an exhaust stroke where the piston 5 ascends.
- 15

- Referring to Fig. 2, the valve train V provided on the cylinder head 3 includes a single camshaft 20 which is rotatably supported on the cylinder head 3 in such a manner as to have a rotational center line L2 which is parallel to the rotational center line of the crankshaft, and further includes an inlet cam 21 which is a primary valve operating cam provided on the camshaft 20 so as to

rotate together with the camshaft 20 and exhaust cams 22
(refer to Fig. 3) which constitutes a pair of secondary
valve operating cams, an inlet operation mechanism for
actuating the inlet valves 14 to be opened and closed in
5 response to the rotation of the inlet cam 21, and an
exhaust operation mechanism for actuating the exhaust
valves 15 to be opened and closed in response to the
rotation of the exhaust cams. Then, in this embodiment,
the inlet operation mechanism is made up of variable
10 properties mechanism which can control the valve
operating properties including opening and closing
timings and maximum lift of the inlet valves 14 in
accordance with the operating state of the internal
combustion engine E.

15 Referring to Figs. 2 to 4, the camshaft 20, which is
situated between the inlet valves 14 and the exhaust
valves 15 in an orthogonal direction A2 relative to the
reference plane H1, which intersects at right angles with
the reference plane H1 and which is situated closer to a
20 lower wall of the valve chamber 16, is supported
rotatably on a camshaft holder which is provided
integrally on the cylinder head 3. The camshaft holder
has a plurality of, here, five, bearing portions 23 which
are provided on the cylinder head 3 at certain intervals
25 in a rotational center line direction A3. Each bearing

portion 23 is made up of a bearing wall 23a which is formed integrally on the cylinder head 3 and a bearing cap 23b which is connected to the bearing wall 23a. The camshaft 20 is driven to rotate at half crankshaft 5 rotational speed, while interlocked therewith, by virtue of the power of the crankshaft which is transmitted via a valve operating transmission mechanism including a chain which is an endless transmission belt extended between a shaft end portion of the crankshaft and a shaft end portion of the camshaft 20. Consequently, the camshaft 10 20, the inlet cams 21 and the exhaust cams 22 rotate in synchronism with the rotation of the crankshaft, which is the rotation of the engine. In addition, the single inlet cam 21 is disposed between the pair of exhaust cams 15 22 in the rotational center line direction A3.

The exhaust operation mechanism includes a transmission mechanism Me which transmits a valve drive force of the exhaust cam 22 to each exhaust valve 15 so as to actuate the exhaust vale 15 to be opened and closed. The transmission mechanism Me includes a rocker shaft 24 as a single support shaft which is disposed directly above the camshaft 20 so as to be in parallel with the camshaft 20 and to intersect at right angles with the reference plane H1 and which is fixedly 20 supported on each bearing cap 23b and exhaust rocker arms

25 which are tertiary rocker arms as a pair of tertiary oscillating members. Each rocker arm 25, which is supported in an oscillatory fashion at a fulcrum portion 25c on the rocker shaft 24 functioning as a pivot support 5 portion, abuts with the exhaust cam 22 via a roller 26 possessed by a cam abutment portion 25a which is made up of an end portion of the exhaust rocker arm 25 and abuts with a valve stem 15a as a valve shaft of the exhaust valve 15 via an adjustment screw 27 possessed by a valve 10 abutment portion 25b which is made up of the other end portion the exhaust rocker arm 25. Here, in the exhaust rocker arm 25, the valve abutment portion 25b is a location positioned closer to the exhaust valve 15 and is also a location positioned on an extension of a valve 15 spring 13 in a direction in which the valve spring 13 extends and contracts (a direction in parallel with an axis L8, which will be described later on). Then, in the exhaust rocker arm 25, the fulcrum portion 25c is provided at an intermediate portion, which is a location 20 between the cam abutment portion 25a and the cam abutment portion 25b. The adjustment screw 27 and an adjustment screw 65, which will be described later on, are such as to adjust the valve clearance to an appropriate value.

The inlet operation mechanism includes a 25 transmission mechanism Mi for transmitting a valve drive

force F_1 (refer to Fig. 6) of the inlet cam 21 to each inlet valve 14 so as to actuate the inlet valve 14 to be opened and closed and a drive mechanism M_d having an electric motor 28 as an actuator for driving a movable holder 30 provided on the transmission mechanism M_i , whereby the valve operating properties of the inlet valve 14 are controlled in accordance with the shift position of the holder 30 which is driven to shift by the drive mechanism M_d .

The transmission mechanism M_i includes the holder 30 which is supported in such a manner as to oscillate about the holder oscillating center line L_3 which is parallel to the rotational center line L_2 relative to the cylinder head 3 so as to oscillate in response to the operation of the electric motor 28, a primary rocker arm 50 as a primary oscillating member which is supported in such a manner as to oscillate about the primary oscillating center line L_4 so as to oscillate in response to the rotation of the inlet cam 21 and a secondary rocker arm 60 as a secondary oscillating member which is supported on the holder in such a manner as to oscillate about the secondary oscillating center line L_5 so as to oscillate in response to the oscillation of the primary rocker arm 50. The secondary rocker arm 60 transmits the valve drive force F_1 transmitted thereto via the primary rocker

arm 50 to the inlet valve 14. Therefore, in this embodiment, an inlet rocker arm for actuating the inlet valve 14 to be opened and closed is made up of a plurality of rocker arms, here, a group of rocker arms 5 which is made up of the primary and secondary rocker arms 50, 60.

The drive mechanism Md includes the electric motor 28, which is mounted on the cylinder head cover 4 outside the valve chamber 16, and the drive shaft 29 which is 10 supported in such a manner as to oscillate relative to the cylinder head 3 so as to be driven to rotate by the reversible electric motor 28 to thereby oscillate the holder 30.

Here, the primary and secondary oscillating center 15 lines L4, L5 and a rotational center line L6 of the drive shaft 29 are parallel to the holder oscillating center line L3, which differs from the rotational center line L2 of the inlet cam 21 and the exhaust cam 22. In addition, the holder oscillating center line L3 and the rotational center line L2 are situated on the inlet side, whereas 20 the rotational center line L6 is situated on the exhaust side.

Referring to Figs. 2, 3, the holder 30, which is disposed between the pair of bearing portions 23 which 25 are adjacent to each other in the rotational center line

direction A3 above the camshaft 20 for each cylinder 1, includes a fulcrum portion 31 which is situated on the inlet side of the cylinder head 3 and is pivot supported on the bearing cap 23b, a gear portion 32 as an acting 5 portion which is situated on the exhaust side of the cylinder head 3 and on which the drive force of the electric motor 28 acts via the drive shaft 29 and primary and secondary support portions 33, 34 which are disposed between the holder oscillating center line L3 and the 10 gear portion 32 in the orthogonal direction A2 and which support the primary and secondary rocker arms 50, 60, respectively. In addition, almost the whole of the transmission mechanism Mi is disposed within an triangle having the rotational center line L2, the holder 15 oscillating center line L3 and the rotational center line L6 as three vertexes thereof (refer to Fig. 2) when viewed from the rotational center line direction A3 (hereinafter, referred to as *when viewed sideways*).

The holder 30, which appears something like an L-shape which bends downwardly toward the inlet cam 21 when 20 viewed sideways, has an arm-like base portion 41 which extends linearly from the holder oscillating center line L3 toward the gear portion 32 and a projecting portion 42 which projects from the base portion 41 in a direction to 25 approach the inlet cam 21. The base portion 41 is made

up of a pair of side walls 43 which face each other in
the rotational center line L3 and a part 44a of a
connecting wall 44 which connects the two side walls 43
together and which makes up an outermost end portion of
5 the holder 30 in a radial direction which radiates from
the holder oscillating center line L3 as a center. In
addition, the projecting portion 42 is made up of a pair
of projecting walls 45 extending downwardly from the
respective side walls 43 and the remaining part 44b of
10 the connecting wall 44 which connects the pair of
projecting walls 45 at portions thereof which are
situated closer to the base portion 41.

The base portion 41 is disposed above the camshaft
20, the inlet cam 21 and the rocker shaft 24 in such a
15 manner as to extend substantially in the orthogonal
direction A2 from the inlet side to the exhaust side, the
fulcrum portion 31 is disposed substantially at the same
position as a valve abutment portion, which will be
described later on, in the orthogonal direction A2, and
20 the holder oscillating center line L3 is disposed on an
extension (in Fig. 2, the extension is shown by chain
double-dashed lines) of a valve stem 14a as a valve shaft
of the inlet valve 14 which extends along an axis L7 of
the valve stem 14a. By adopting this construction, a
25 distance between the holder oscillating center line L3

and a line of action of a reaction force F2 (refer to Fig. 6) from the inlet valve 14 is maintained small within the range of the valve stem 14a as a maximum limit. On the other hand, the projecting portion 42, which is disposed to extend substantially in the cylinder axis direction A1, is always situated on the exhaust side within the oscillating range of the holder 30.

The fulcrum portion 31 and the secondary support portion 34 are provided on each side wall 43, the gear portion 32 is provided on the connecting wall 44 in such a manner as to extend from the base portion 41 to the projecting portion 42, and the primary support portion 33 is provided on each projecting wall 45. As shown in Fig. 4, the fulcrum portion 31 is pivot supported on a support portion 23c formed on the bearing cap 23b. The support portion 23c defines a hole 71 having a circular section in cooperation with a holding cap 70 connected to an upper end portion of the bearing cap 23b with a bolt, so that a support shaft 31a formed on the fulcrum portion 31 is inserted into the hole 71 in such a manner as to slide therein. Then, a support shaft 31a of a holder 30 belonging to the adjacent cylinder 1 is supported on the common gearing cap 23b.

Referring to Fig. 2, in a lower side portion of each side wall 43 which constitutes a lower side portion of

the base portion 41, a portion on the camshaft 20 side where the projecting wall 45 projects downwardly from the side wall 43 forms an accommodating portion 39 which defines an accommodating space 39a for accommodating 5 therein the holder 30 and the rocker shaft 24 which is a member disposed on the periphery of the primary rocker arm 50 in cooperation with a portion of the projecting wall 45 which is closer to the side wall 43. The accommodating space 39a opens downwardly toward the 10 rocker shaft 24. Then, a ratio at which the rocker shaft 24 is accommodated in the accommodating space 39 becomes maximum when the rocker shaft 24 occupies a primary limit position as a predetermined position which is an oscillation position resulting when the holder 30 15 oscillates most downwardly (a state shown in Fig. 2 or Fig. 6).

Referring to Fig. 3, as well, in the base portion 41, a portion excluding the fulcrum portion 31 is disposed between the pair of exhaust rocker arms 25 in 20 the rotational center line direction A3, and the primary and secondary rocker arms 50, 60 are disposed between the pair of side walls 43 in the rotational center line direction A3. The primary support portion 33 and the primary oscillating center line L4 are situated on the 25 exhaust side, whereas the secondary support portion 34

and the secondary oscillating center line L5 are situated on the inlet side. Then, the distance to the holder oscillating center line L3 gets longer in the order of the secondary oscillating center line L5, the rotational center line L2, the primary oscillating center line L4 and the rotational center line L6. Therefore, as shown in Fig. 2, with a primary intersection point C1 between the orthogonal plane and the primary oscillating center line L4 and a secondary intersection point C2 between the orthogonal plane and the secondary oscillating center line L5, a distance between the holder oscillating center line L3 and the primary intersection point C1 is longer than a distance between the holder oscillating center line L3 and the secondary intersection point C2.

In addition, in the oscillating range of the holder 30, the primary oscillating center line L4 includes the holder oscillating center line L3 and is situated on a camshaft side where the camshaft 20 is situated or a lower side relative to a specific plane H2 which intersects at right angles with the reference plane H1, whereas the secondary oscillating center line L5 is situated on an opposite side to the camshaft side or an upper side. In this embodiment, when the holder 30 occupies a secondary limit position as a predetermined 25 position which is an oscillation position resulting when

the holder 30 oscillates most upwardly (a state shown in chain double-dashed lines in Fig. 1, or a state shown in Fig. 7), the primary oscillating center line L4 is situated substantially on the specific plane H2 and is 5 situated below the specific plane H2 when the holder 30 occupies any other position than the secondary limit position.

The primary support portion, which regulates the primary oscillating center line L4, is provided on a 10 lower end portion of the projecting portion 42 which constitutes a location closer to the inlet cam 21 and has a cylindrical support shaft 35 which is press fitted into a hole formed in each side wall 43. The primary rocker arm 50, which is supported by the support shaft 35 at a 15 fulcrum portion 51 in an oscillatory fashion via a multiplicity of needles 36, abuts with the inlet cam 21 at a roller 53 possessed by a cam abutment portion 52 made up of one end portion of the primary rocker arm 50 and abuts with the secondary rocker arm 60 at a drive 20 abutment portion 54 made up of the other end portion thereof. In the primary rocker arm 50, the fulcrum portion 51 is provided at an intermediate portion which is a location between the cam abutment portion 52 and the drive abutment portion 54. Then, the primary rocker arm 25 50 is biased by virtue of a biasing force of a biasing

device (not shown) such as a spring held by the holder 30 such that the roller 53 is pressed against the inlet cam 24 at all times. In addition, an accommodation space 57 for accommodating therein the roller 53 is provided in 5 the primary rocker arm 50 in such a manner as to extend from the fulcrum portion 51 to the cam abutment portion 52, and the accommodation space 57 constitutes an escape space which allows the passage of a cam lobe portion 21b of the rotating inlet cam 21. Then, the primary rocker 10 arm 50 and the inlet cam 24 can be disposed close to each other, while the interference of the primary rocker arm 50 with the inlet cam 24 is avoided by the accommodation space 57.

The secondary support portion 34, which regulates 15 the primary oscillating center line L5, is provided on the base portion 41 so as to be situated between the primary support portion 33 and the holder oscillating center line L3 in the orthogonal direction A2 and has a support shaft 37 which is press fitted into a hole formed 20 in each side wall 43. The secondary rocker arm 60, which is supported by the support shaft 37 at a fulcrum portion 61 in an oscillatory fashion via a multiplicity of needles 38, abuts with the drive abutment portion 54 of the primary rocker arm 50 at a roller 63 possessed by a 25 follower abutment portion 62 made up of one end portion

of the secondary rocker arm 60 and abuts with the valve
stems 14a as the abutment portions of the pair of inlet
valves 14, respectively, at adjustment screws 65
possessed by a pair of valve abutment portions 64 made up
5 of the other end portion thereof. Here, in the secondary
rocker arm 60, the valve abutment portion 64 is a
location which is situated closer to the inlet valve 14
and is also a location which is situated on an extension
of the valve spring 13 in a direction (a direction
10 parallel to the axis L7) in which the valve spring 13
extends and contracts. Then, in the secondary rocker arm
60, the fulcrum portion 61 is provided on an intermediate
portion which is a location between the follower abutment
portion 62 and the valve abutment portion 64. In
15 addition, since the sectional shape of the roller 63 is
of a circular shape, the sectional shape of an abutment
surface of the follower abutment portion 62, which is
brought into abutment with a cam profile 55, which will
be described later, is of an arc-like shape, as well.
20 On the drive abutment portion 54 acting as one of
the drive abutment portion 54 and the follower abutment
portion 62 which are brought into abutment with each
other, the cam profile 55 is formed, which cam profile 55
has a lost motion profile 55a which maintains the inlet
25 valve 14 in a closed state and a drive profile 55b which

puts the inlet valve 14 in an opened state through the abutment with the roller 63 of the follower abutment portion 62 which acts as the other abutment portion.

Then, an arm abutment position P2, which is an abutment position where the cam profile 55 and the roller 63 abut with each other, resides above the camshaft 20 and the rocker shaft 24 and is situated at a position which is superposed above the camshaft 20 and the rocker shaft when viewed from the cylinder axis direction A1

10 (hereinafter, referred to as when viewed from the top).

The lost motion profile 55a is formed so as to have an arc-like sectional shape which is formed about the primary oscillating center line L4 and is designed such that the valve drive force F1 of the inlet valve 21 which

15 is transmitted via the primary rocker arm 50 is not transmitted to the secondary arm 60 in a state in which a clearance is formed between the lost motion profile 55a and the roller 63, as well as in a state in which the roller 63 is in abutment with the lost motion profile

20 55a. As this occurs, the primary rocker arm 50 is in a rest state where the secondary rocker arm 60 is not oscillated by the inlet cam 21 via the primary rocker arm 50. Then, when the primary rocker arm 50 and the secondary rocker arm 60 are brought into abutment with

25 each other in a state where the roller 53 of the primary

rocker arm 50 is in abutment with a base circle portion
21a of the inlet cam 21, the roller 63 abuts with the
lost motion profile 55a at all times. Consequently, when
the arm abutment position P2 is located at an arbitrary
5 position on the lost motion profile 55a, the inlet valve
14 is maintained in the closed state by virtue of the
spring force of the valve spring 13, and a valve
clearance is formed between a valve abutment surface 65a
of the adjustment screw 65 which acts as a valve abutment
10 surface of the valve abutment portion 64 and a distal end
surface 14b of the valve stem 14a which acts as an
abutment surface of the inlet valve 14.

The drive profile 55b transmits the valve drive
force F1 of the inlet cam 21 which is transmitted thereto
15 via the primary rocker arm 50 to the secondary rocker arm
60 so as to oscillate the secondary rocker arm 60, and
when the adjustment screw 65 is in abutment with the
valve stem 14a, the secondary rocker arm 60 which is
oscillating transmits the valve drive force F1 to the
20 inlet valve 14 to thereby put the inlet valve 14 into an
opened state with a predetermined lift amount being
provided.

Consequently, the oscillating position of the
secondary rocker arm 60 relative to the holder 30 is
25 regulated by the primary rocker arm 50.

In addition, the drive abutment portion 54 has a pent roof-like thin portion 54a which projects diagonally downwardly toward the inlet cam 24 or the inlet valve 14, and the lost motion profile 55a is formed on the thin portion 54a. Then, an accommodation portion 56 in which the rocker shaft 24 is accommodated in accordance with the oscillating position thereof is formed by making use of the thin portion 54a in the primary rocker arm 50 between the primary oscillating center line L4 and the lost motion profile 55a in a radial direction which radiates from the primary oscillating center line L4 as a center. Then, as the holder 30 approaches the primary limit position and the primary rocker arm 50 oscillates in a direction in which the lift amount of the inlet valve 14 is increased, the ratio at which the rocker shaft 24 is accommodated in the accommodation portion 56 is increased.

The sectional shape of the valve abutment surface 65a of the adjustment screw 65 which abuts with the distal end surface 14b of the inlet valve 14 is an arc that is formed about the holder oscillating center line L3 when in a state where the cam profile 55 of the primary rocker arm 50 and the roller 63 of the secondary rocker arm 60 are in abutment with each other and a state where the secondary rocker 60 is in the rest state, that

is, a state where the roller 63 abuts with the lost motion profile 55a. Due to this, the valve abutment surface 65a is made up of a partially cylindrical surface which is part of a cylindrical surface that is formed about the holder oscillating center line L3 or a partially spherical surface which is part of a spherical surface that is formed about a point on the holder oscillating center line 3 when in a state the secondary rocker arm 60, which is in the rest state, abuts with the lost motion profile 55a. Then, the secondary rocker arm 60, when in the rest state, does not oscillate relative to the holder 30 irrespective of the oscillating position of the holder 30 in the state where the roller 63 of the secondary rocker arm 60 does not abut with the lost motion profile 55a of the primary rocker arm 50.

The pair of fulcrum portions 31 on the base portion constitutes an accommodation space in which the pair of valve abutment portions 64 provided in series in the rotational center line direction A3 and the pair of adjustment screws 65 are accommodated.

Furthermore, when the primary rocker arm 60 is in the rest state so as to maintain the inlet valve 14 in the closed state, the fulcrum portion 31 is situated at a position where the fulcrum portion 31 is superposed on the valve abutment portion 64 and the adjustment screw 65

when viewed sideways, and the holder oscillating center line L3 is situated at a position where the holder oscillating center line L3 intersects at right angles with the valve abutment portion 64 and, furthermore, the 5 adjustment screw 65, and more precisely, the holder oscillating center line L3 is situated at a position where it intersects at right angles with the center axis of the adjustment screw 65.

In addition, the primary rocker arm 50 is disposed 10 in such a manner as to extend long in the cylinder axis direction A1 and is situated on the exhaust side except for the drive abutment portion 54 within the oscillating range of the holder, the cam abutment position P1 which is the abutment position where the roller 53 abuts with 15 the inlet cam 21 is situated on the exhaust side, and the arm abutment position P2 is situated on the inlet side. Then, the roller 53 abuts with the inlet cam 21 at a portion which is closer to the exhaust valve 15 in the orthogonal direction A2, and when the holder 30 20 oscillates, the cam abutment position P1 shifts mainly in the cylinder axis direction A1. On the other hand, the secondary rocker arm 60 is disposed in such a manner as to extend long in the orthogonal direction A2 and along the base portion 41 and is situated at on the inlet side 25 within the oscillating range of the holder 30.

Referring to Fig. 4, as well, the drive shaft 29 is a single rotating shaft which is common to all the cylinders 1 in the orthogonal direction A2 and is rotatably supported on the bearing caps 23b at journal portions 29a thereof by means of holding caps 72 which are connected to the bearing caps 23a with bolts to thereby be rotatably supported on the cylinder head 3.

Drive gears 29b are provided on the drive shaft 29 at certain intervals in the rotational center line direction A3 for each cylinder 1, and the drive gear 29b meshes with the gear portion 32 formed in the connecting wall 44 so as to oscillate the holder 30 about the holder oscillating center line L3 by virtue of the torque of the electric motor 28.

The gear portion 32 is a surface on the connecting wall 44 constituting part of the base portion 41 and the projecting portion 42 which surface faces the drive shaft 29 and is formed to extend between the base portion 41 and the projecting portion 42 on an outer circumferential surface 44c in a radial direction which radiates from the holder oscillating center line L3 as a center. This outer circumferential surface 44c constitutes a location of the holder 30 which is farthest apart from the holder oscillating center line L3. The gear portion 32 is formed such that the shape thereof on the orthogonal

plane becomes an arc-like shape which is formed about the holder oscillating center line L3 and has a number of teeth which are arranged in an arc-like fashion on the orthogonal plane. Then, a line of action of a drive force exerted from the drive shaft 29 so as to act on the gear portion 32 is directed in a tangential direction to an arc that is formed about the holder oscillating center line L3 on the orthogonal plane.

In addition, the drive shaft 29 is situated on an extension of a valve stem 15a of the exhaust valve 15 which extends along an axis L8 of the valve stem 15a, and most of the whole of drive shaft 29 is situated closer to the reference plane H1 than the extension of the valve stem 15a. In addition, in the orthogonal direction A2, the drive shaft 29 is situated substantially at the same position as those of the valve abutment portion 25b of the exhaust rocker arm and a distal end face 15b of the valve stem 15a. Due to this, as shown in Fig. 4, when viewed from the top, the drive shaft 29 is situated at a position which is superposed above the valve abutment portion 25b and the distal end face 15b. Here, in the exhaust valve 15, the valve stem 15a is an abutment portion with which the valve abutment portion 25 is brought into abutment, and the distal end face 15b is an abutment surface of the abutment portion.

The electric motor 28 is controlled by an electronic control unit (hereinafter, referred to as *ECU*) into which detection signals from operating conditions detecting units for detecting operating conditions of the internal combustion engine E are inputted. The operating conditions detecting units include a rotational speed detecting unit for detecting the engine rotational speed of the internal combustion engine E, a load detecting unit for detecting the load of the internal combustion engine E and the like. Then, by controlling the rotational direction and rotational speed of the electric motor 28 according to the operating conditions by the ECU, the rotational direction and rotational amount of the drive shaft 29 are controlled, whereby the holder 30 is driven to oscillate within the oscillating range which is regulated between the primary limit position and the secondary limit position by the electric motor 28, irrespective of the rotational position of the inlet cam 21 or the camshaft 20. Then, the primary rocker arm 50 having the primary center line L4 which oscillates together with the holder 30 and the secondary rocker arm 60 having the secondary oscillating center line L5 shift, respectively, in accordance with the oscillating position of the holder that is controlled in accordance with the operating conditions, whereby the opening and closing

timings, maximum lift amount and maximum lift timing are changed continuously.

In addition, as shown in Fig. 3, the holder 30, the primary and secondary rocker arms 50, 60 and the drive gear 29b are formed so as to be substantially symmetrical with respect to plane relative to a plane H3 which contains a central point which bisects the width of the primary rocker arm 50 in the rotational center line direction A3 and intersects at right angles with the 10 holder oscillating center line L3. Consequently, since in the transmission mechanism Mi, there is generated no moment acting around a straight line which intersects at right angles with the reference plane H1 based on the valve drive force F1, the reaction force F2 from the 15 inlet valve 14 and the drive force of the drive shaft 29, an increase in abutment pressure that is generated locally at a sliding portion by the moment is prevented, thereby the durability of the transmission mechanism Mi being increased.

20 Next, referring to Figs. 5 to 8, the valve operating properties will be described below that can be obtained by the inlet operation mechanism.

Referring to Fig. 5, the valve operating properties are changed between a maximum valve operating property Ka 25 and a minimum valve operating property Kb continuously

with the maximum valve operating property K_a and the minimum valve operating property K_b acting as limit properties, whereby a countless number of intermediate valve operating properties K_c can be obtained between 5 both the valve operating properties K_a , K_b . For example, the opening and closing timings and maximum valve lift amount of the inlet valve 14 changes as will be described below from the maximum valve operating property K_a which is a valve operating property resulting when the internal 10 combustion engine E is operated in a high rotational speed region or high load region to the minimum valve operating property K_b via the intermediate valve operating properties K_c which are valve operating properties resulting when the internal combustion engine 15 E is operated in a low rotational speed region or low load region via. The valve opening timing is delayed continuously, whereas the valve closing timing is advanced continuously in a large changing amount when compared with the opening timing so that the valve 20 opening period becomes short continuously, and furthermore, the maximum lift timing where the maximum lift amount can be obtained is advanced continuously, and the maximum lift amount becomes small continuously. Note that the maximum lift timing is introduced to a timing 25 which bisects the valve timing period.

In addition, in this embodiment, the minimum valve operating property is a valve operating property where a valve rest state can be obtained where the maximum lift amount becomes zero and the opening and closing operation 5 of the inlet valve 14 comes to rest.

In the valve operating properties that can be obtained by the inlet operation mechanism, in the maximum valve operating property K_a , the valve opening period and the maximum lift amount become maximum, and the valve 10 closing timing is introduced to a timing where it is most delayed. The maximum valve operating property K_a can be obtained when the holder 30 occupies the primary limit position as shown in Fig. 2, 6. Note that in Figs. 6 to 15, the transmission mechanism M_i is shown in solid lines which results when the inlet valve 14 is in the closed state, whereas the transmission mechanism M_i is shown in chain double-dashed lines which results when the inlet valve 14 is opened in the maximum lift amount.

Referring to Fig. 6, when situated at the primary 20 limit position, the holder 30 occupies an oscillating position which is closest to the rotational center line L_2 or the inlet cam 21 within the oscillating range, and the primary support portion 33 is situated so as to be superposed above the cam lobe portion 21b of the inlet 25 cam 21 in the cylinder axis direction A_1 . The roller 63

of the secondary rocker arm 60 is in a state where the roller 63 abuts with the lost motion profile 55a of the cam profile 55 in a state where the roller 53 of the primary rocker arm 50 abuts with the base circle portion 21a of the inlet cam 21. As this occurs, the rocker shaft 24 is accommodated in the accommodation space 56a at a relatively small ratio. When the primary rocker arm 50 is brought into abutment with the cam lobe portion 21b to thereby be caused to oscillate in a counter-rotational direction R2 (a direction opposite to the rotational direction R1 of the inlet cam 21) by virtue of the valve drive force F1, the drive profile 55b abuts with the roller 63, so that the secondary rocker arm 60 is caused to oscillate in the counter-rotational direction R2, whereby the secondary rocker arm 60 opens the inlet valve 14 against the spring force of the valve spring 13.

Then, the rocker shaft 24 is accommodated in the accommodation space 56a at a maximum ratio.

On the other hand, the minimum valve operating property Kb can be obtained when the holder 30 occupies the secondary limit position as shown in Fig. 7. In the minimum valve operating property Kb, irrespective of the fact that the primary rocker arm 50 is caused to oscillate by virtue of the valve drive force F1 of the inlet cam 21, the roller 63 is in the state where the

roller 63 abuts with the lost motion profile 55a, and the secondary rocker arm 60 is in the rest stage. The holder 30, which is situated at the secondary limit position, occupies a farthest oscillating position from the 5 rotational center line L2 or the inlet cam 21 within the oscillating range.

In addition, when the holder 30 occupies a central position which is substantially the center of the oscillating range, as shown in Fig. 8, as an oscillating 10 position between the primary limit position and the secondary limit position, an intermediate valve operating property K_{c1} can be obtained as one of a countless number of intermediate valve operating properties K_c between the maximum valve operating property K_a and the minimum valve 15 operating property K_b , as shown in Fig. 5. In the intermediate valve operating properties K_c , when compared with the maximum valve operating property K_a , the valve opening period and maximum lift amount become small, and the opening timing is introduced to a timing where it is delayed, whereas the closing timing and the maximum lift 20 timing are introduced to a timing where they are advanced.

Thus, in the valve train V, as the maximum lift amount becomes smaller, while the opening timing is delayed in a relatively small changing amount, the 25

closing timing and the maximum lift timing are advanced
in a relative large changing amount when compared with
the opening timing, whereby the inlet valve 14 is closed
earlier. Due to this, when the internal combustion
5 engine E is operated in the low rotational speed region
or low load region, the inlet valve 14 is operated to be
opened and closed in a small lift amount region where the
maximum lift amount is small, and the valve operating
properties are controlled so that the closing timing of
10 the inlet valve 14 is advanced, whereby a pumping loss is
reduced to thereby increase the fuel consumption
performance by implementing an earlier closing of the
inlet valve 14.

Next, referring to Figs. 5, 6, 7, the operation of
15 the transmission mechanism Mi will be described below
which results when the holder 30 oscillates from the
primary limit position to the secondary limit position.

When the drive force of the drive shaft 29 driven by
the electric motor 28 acts on the gear portion 32,
20 whereby the holder 30 oscillates upwardly from the
primary limit position in an oscillating direction (in
the counter-rotational direction R2) in which the holder
30 moves apart from the rotational center line L2, the
cam abutment position P1 shifts in the counter-rotational
direction R2, and at the same time the primary and
25

secondary oscillating center lines L4, L5 oscillate together with the holder 30 so that the arm abutment position P2 shifts in a direction in which the maximum lift amount of the inlet valve 14 is decreased and in a 5 direction to move apart from the rotational center line L2, whereby the primary and secondary rocker arms 50, 60 oscillate around the primary and secondary oscillating center lines L4, L5, respectively. In Fig. 7, L4a, L5a, P1a and P2a denote, respectively, primary and secondary 10 oscillating center lines, a cam abutment position and an arm abutment position when the holder occupies the primary limit position.

When the primary oscillating center line L4 oscillates, the cam abutment position P1 shifts in the 15 counter-rotational direction R2, and the timing when the roller 53 is brought into abutment with the cam lobe portion 21b is advanced, while the drive abutment portion 54 shifts in a direction in which a shift range of the arm abutment position P2 on the lost motion profile 55a 20 (a range of the rotational angle of the camshaft 20 or a range of the crank angle of the crankshaft) is increased in a state where the roller 53 is in abutment with the base circle portion 21a. Then, even in the event that the shift range of the arm abutment position P2 on the 25 lost motion profile 55a is expanded, so that the arm

abutment position R2 is brought into abutment with the cam lobe portion 21b, whereby the primary rocker arm 50 starts to oscillate, since the roller 63 stays on the lost motion profile 55a, the secondary rocker arm 60 is 5 in the rest state, and when the inlet cam 21 rotates further so that the primary rocker arm 50 is caused to oscillate more largely, whereby the roller 63 is brought into abutment with the drive profile 55b, the secondary rocker arm 60 oscillates largely, whereby the inlet valve 10 14 is opened. Due to this, even with the roller 63 being in abutment with an apex 21blof the cam lobe portion 21, the oscillating amount of the secondary rocker arm 60 that is caused to oscillate by the drive profile 55b is reduced when compared with when at the primary limit 15 position, whereby the maximum lift amount of the inlet valve 14 is reduced. Then, in this embodiment, the shape of the inlet cam 21, the shape of the cam profile 55, and the positions of the primary and secondary oscillating center lines L4, L5 are set such that when the holder 20 oscillates from the primary limit position toward the secondary limit position, while the opening timing of the inlet valve 14 is, as shown in Fig. 5, delayed in a relatively small changing amount, the closing timing and maximum lift amount of the inlet valve 14 are advanced in 25 a larger changing amount than the changing amount of the

opening timing.

In addition, the valve operating properties are controlled such that when the holder 30 oscillates from the secondary limit position toward the primary limit 5 position in such a manner as to approach the rotational center line L2, the opening timing of the inlet valve 14 advances continuously from the minimum valve operating property Kb to the maximum valve operating property Ka, whereas the closing timing is delayed continuously, so 10 that the valve opening period is extended continuously, and furthermore, the maximum lift amount timing is delayed continuously and the maximum lift amount is increased continuously.

In addition, as is clear from Figs. 6, 7, since, 15 when the oscillating position of the holder 30 is situated at the primary limit position where the maximum valve operating property Ka can be obtained where the maximum lift amount becomes maximum, the cam abutment position P1 where the roller 53 of the cam abutment portion 52 abuts with the cam lobe portion 21b of the inlet cam 21 is situated at a position close to a specific straight line L10 which passes through the holder oscillating center line L3 and the rotational center line L2 on the orthogonal plane which intersects 20 the holder oscillating center line L3 and the rotational center line L2 on the orthogonal plane which intersects 25 the holder oscillating center line L3 and the rotational center line L2 on the orthogonal plane which intersects

L3 when compared with when the holder 30 occupies the secondary limit position where the minimum valve operating property K_b can be obtained where the maximum lift amount becomes smallest, as the holder 30 approaches 5 the primary limit position where the valve drive force is increased, the cam abutment position P1 where the roller 53 abuts with the cam lobe portion 21b approaches the specific straight line L10 on the orthogonal plane.

Next, referring to Fig. 7, the operation of the 10 primary and secondary rocker arms 50, 60 will be described below which results when the holder 30 oscillates within the oscillating range.

Since the primary and secondary rocker arms 50, 60 shift in accordance with the oscillating positions of the 15 primary and secondary oscillating center lines L4, L5 which oscillate together with the holder, the relative position of the primary and secondary oscillating center lines L4, L5 on the holder 30 remains unchanged, and moreover, since the sectional shape of the lost motion 20 profile 55a is the arc-like shape which is formed about the primary oscillating center line L4, the positional relationship among the three members such as the primary and secondary oscillating center lines L4, L5 and the arm abutment position P2 remains unchanged irrespective of 25 the oscillating position of the holder 30 when the lost

motion profile 55a and the roller 63 are in the abutment state where the two members abut with each other.

In addition, since the primary and secondary oscillating center lines L4, L5 oscillate together with the holder 30, the control range of the valve operating properties can be set large by increasing the shift amount of the cam abutment position P1. For example, in order to obtain the same abutment position as the arm abutment position relative to the lost motion profile 55a, as with primary and secondary rocker arms n1, n2 shown in chain triple-dashed lines in Fig. 7, a primary oscillating center line N3 shifts, and when compared with a case where while a primary oscillating center line n3 shifts, a secondary oscillating center line n4 does not shift, in this transmission mechanism Mi, the shift amount of the cam abutment position P1 can be increased. As a result, when compared with the conventional example, the opening and closing timings of the inlet valve 14 can be changed in a large oscillating amount. Then, even in the event that the holder oscillates in a large oscillating amount so that the control range of the valve operating properties is set large, the relative shift amount of the arm abutment position P2 with the roller on the cam profile 55a can be suppressed to a small level.

Next, the function and advantage of the embodiment

constructed as has been described heretofore will be described below.

The transmission mechanism Mi includes the primary and secondary rocker arms 50, 60 which have, respectively, the drive abutment portion 54 and the follower abutment portion 62 which abut with each other and the holder 30 which is caused to oscillate around the holder oscillating center line L3 by the electric motor 28 and which support the primary and secondary rocker arms 50, 60 in an oscillatory fashion so that the primary and secondary oscillating center lines L4, L5 oscillate together. The cam profile 55 having the lost motion profile 55a and the drive profile 55b is formed on the drive abutment portion 54, and since the sectional shape of the lost motion profile 55a on the orthogonal plane which intersects at right angles with the primary oscillating center line L4 is the arc-like shape which is formed about the primary oscillating center line L4, the relative position of the primary and secondary oscillating center lines L4, L5 in the holder 30 remains unchanged, when the valve operating properties are changed through the shift of the primary and secondary rocker arms 50, 60 in accordance with the oscillating positions of the primary and secondary oscillating center lines L4, L5 which rotate together with the holder 30.

Moreover, since the sectional shape of the lost motion profile 55a is the arc-like shape which is formed about the primary oscillating center line L4, it becomes easy to maintain the clearance formed between the lost motion profile 55a and the roller 63 or the abutment state

5 profile 55a and the roller 63, thereby making it possible to maintain an appropriate valve clearance even at the time of changing the valve operating properties. Due to this, the increase in noise

10 can be prevented which would otherwise result, for example, from the valve striking noise by virtue of an increase in valve clearance and collision of both the rocker arms 50, 60 with each other. In addition, even in the event that the holder 30, which supports the primary

15 and secondary rocker arms 50, 60, oscillates in a large oscillating amount in order to increase the control range of the valve operating properties, since the primary and secondary oscillating center lines L4, L5 oscillate together with the holder 30, when compared with the case

20 where while one of the primary and secondary oscillating center lines shifts, the other does not, the relative shift amount of the arm abutment position P2 can be suppressed to a small level, and therefore, also in this case, it becomes easy to maintain the clearance between

25 the cam profile 55a and the roller 63 or the abutment

state therebetween, thereby making it possible to set large the control range of the valve operating properties.

The secondary rocker arm 60 has the valve abutment portion 64 which has, in turn, the valve abutment surface 65a which is brought into abutment with the inlet valve 14, and the distance between the primary oscillating center line L4 and the holder oscillating center line L3 is longer than the distance between the secondary oscillating center line L5 and the holder oscillating center line L3, whereby since the valve drive force F1 of the inlet cam 21 is transmitted to the inlet valve 14 only through the primary and secondary rocker arms 50, 60, the transmission mechanism Mi is made compact in size, and hence the valve train V itself is made compact in size. Due to this, the cylinder head 3 on which the valve train V is provided becomes compact in size. In addition, when the holder 3 oscillates, since the shift amount of the primary oscillating center line L4 becomes larger than that of the secondary oscillating center line L5, the shift amount of the cam abutment position P1 can be increased, and therefore, the control range of the opening closing timings of the inlet valve 14 can be set large. Moreover, since the shift amount of the valve abutment position which is the abutment position where

the valve abutment portion 64 of the secondary rocker arm
60 abuts with the inlet valve 14 can be reduced, the wear
of the valve abutment portion 64 can be suppressed,
thereby making it possible to extend a period of time
5 when the proper valve clearance is maintained.

In the holder 30 having the base portion 41 which
extends from the holder oscillating center line L3 toward
the gear portion 32 substantially in the orthogonal
direction A2 and the projecting portion 42 which projects
10 from the base portion 41 in the direction to approach the
inlet cam 21 substantially in the cylinder axis direction
A1, the primary support portion 33 is provided on the
projecting portion 42 for supporting the primary rocker
arm 50 in an oscillatory fashion, and the secondary
15 support portion 34 is provided on the base portion 41 for
supporting the secondary rocker arm 60 in an oscillatory
fashion. Since the primary and secondary support
portions 33, 34 are disposed between the holder
oscillating center line L3 and the gear portion 32, the
20 gear portion 32 is situated farther than the primary and
secondary support portions 33, 34 relative to the holder
oscillating center line L3, and therefore, the drive
force of the electric motor 28 can be reduced, whereby
the electric motor 28 is made compact in size. Moreover,
25 since the primary support portion 33 and the secondary

support portion 34 are provided on the projecting portion and the base portion separately, the space between the holder oscillating center line L3 and the gear portion 32 can be reduced, whereby the holder 30 is made compact in
5 size between the holder oscillating center line L3 and the gear portion 32. Due to this, the cylinder head 3 on which the valve train V is provided can be made compact in size in the orthogonal direction A2. In addition, since the primary support portion 33 which is provided on
10 the projecting portion 41 is situated closer to the inlet cam 21 than to the base portion 41, in the primary rocker arm 50, when compared with a case where the primary support portion is provided on the base portion 41, the distance between the primary oscillating center line L4 and the cam abutment portion 52 becomes short, a required
15 rigidity against the valve drive force F1 is ensured, while the primary rocker arm 50 is made light in weight.

The accommodation space 39a for accommodating the rocker shaft 24 which supports the exhaust rocker arm 25 is formed in the holder 30, whereby the holder 30 and the
20 rocker shaft 24 can be disposed close to each other, while the interference of the holder 30 with the rocker shaft 24 is avoided, and therefore, the valve train V is made compact in size, and moreover, the oscillating range
25 of the holder 30 can be increased within the limited

space, and therefore, the control range of the valve operating properties can be increased.

In the primary rocker arm 50, the accommodation space 56a for accommodating the rocker shaft 24 which

5 supports the exhaust rocker arm 25 in an oscillatory fashion is formed between the primary oscillating center line L4 and the lost motion profile 55a in the radial direction which radiates from the primary oscillating center line L4 as a center, whereby almost no valve drive force F1 or reaction force F2 from the inlet valve 14 is

10 transmitted to the lost motion profile 55a, and therefore, the rigidity required for the portion of the drive abutment portion 54 where the lost motion profile 55a is formed only has to be small, and the portion can

15 be made thin, and therefore, the primary rocker arm 50 is made light in weight. In addition, the accommodation space 56a is formed by making used of the thin portion 54a. Then, since, by allowing the rocker shaft 24 to be accommodated in the accommodation space 56a, the primary

20 rocker arm 50 and the rocker shaft 24 can be disposed close to each other, while the interference of the primary rocker arm 50 with the rocker shaft 24 is avoided, the valve train V is made compact in size.

Furthermore, by allowing the rocker shaft to also be

25 accommodated in the accommodation space 39a, the primary

rocker arm 50 and the rocker shaft 24 can be disposed close to each other, while the interference of the primary rocker arm 50 with the rocker shaft 24 is avoided, and therefore, the valve train V is made compact
5 in size. In addition, since the oscillating range of the holder 30 which supports the primary rocker arm 50 within the space in the limited valve chamber 16 can be increased, the control range of the valve operating properties can be set large.

10 Due to the primary rocker arm 50 which is in abutment with the inlet cam 24 and the secondary rocker arm 60 being in the state where the primary rocker arm 50 and the secondary rocker arm 60 are in abutment with each other at the abutment portions 54, 63, respectively, the
15 sectional shape of the valve abutment surface 65a of the valve abutment portion 64 provided on the secondary rocker arm 60 having the secondary oscillating center line L5 which oscillates together with the holder 30 on the orthogonal plane which intersects at right angles with the holder oscillating center line L3 is the arc-
20 like shape which is formed about the holder oscillating center line L3 in the state where there exists no clearance in the transmission path of the valve drive force which extends from the inlet cam 21 to the
25 secondary rocker arm 60 via the primary rocker arm 50,

and with the secondary rocker arm 60 being in the rest state where the secondary rocker arm 60 is not caused to oscillate by the inlet cam 21 via the primary rocker arm 50, and therefore, even in the event that the holder 30 5 oscillates about the holder oscillating center line L3 in order to change the valve operating properties, the secondary rocker arm 60 having the secondary oscillating center line L5 which oscillates together with the holder 30 oscillates together with the holder 30, and the clearance between the valve abutment surface 65a and the distal end face 14b of the inlet valve 14 is maintained constant, whereby the valve clearance from the inlet cam 21 to the inlet valve 14 is maintained constant.

The valve abutment portion 64 having the valve 15 abutment surface 65a which is brought into abutment with the distal end face 14b of the inlet valve 14 is provided on the secondary rocker arm 60 at the position which intersects at right angles with the holder oscillating center line L3, whereby the valve abutment surface 65a is 20 allowed to be close to the holder oscillating center line L3, and therefore, even in the event that the secondary oscillating center line L5 oscillates due to the oscillation of the holder 30, whereby the valve abutment position where valve abutment surface 65a abuts with the 25 distal end face 14b is caused to shift, the shift amount

is made to be small, and in this respect, as well, the progress in wear of the valve abutment surface 35a attributed to the oscillation of the holder 30 is suppressed, and then, the period of time when the 5 appropriate valve clearance is maintained is extended.

In addition, the valve abutment surface 65a resides close to the holder oscillating center line L3, whereby the valve abutment portion 64 can be reduced, and therefore, the secondary rocker arm 60 is made small in size.

10 The gear portion 32 on which the drive force of the drive shaft 29 acts is provided on the holder 30 on the outer circumference 44c which is the location of the holder 30 which is farthest apart from the holder oscillating center line L3 on the orthogonal plane,

15 whereby on the holder 30, the distance from the holder oscillating center line L3 to the acting position of the drive force can be made substantially maximum, and therefore, the drive force of the electric motor 28 can be reduced, the electric motor 28 being thereby made

20 compact in size. In addition, the gear portion 32 is provided so as to extend from the base portion 41 to the projecting portion 42, whereby the forming range of the gear portion 32 can be increased, and therefore, the oscillating range of the holder 30 can be increased.

25 When the holder 30 oscillates in the oscillating

direction to move away from the rotational center line L2, the cam abutment position P1 shift in the counter-rotational direction R2, and at the same time the arm abutment position P2 shifts in the direction in which the 5 maximum lift amount of the inlet valve 14 is reduced and in the direction to move away from the rotational center line L2, whereby the closing timing and the maximum lift timing are advanced, and at the same time the valve operating property can be obtained where the maximum lift 10 amount is reduced. As this occurs, although the secondary rocker arm 60 shifts together with the holder in the direction to move away from the rotational center line L2, since at the same time the maximum lift amount of the inlet valve 14 which is actuated to be opened and 15 closed by the secondary rocker arm 60 is reduced, the oscillating amount of the secondary rocker arm 60 is reduced, and therefore, the operating space occupied by the secondary rocker arm 60 is made compact by that extent, thereby making it possible to disposed the valve 20 train V in a relatively compact space.

In the event that the abutment state where the inlet cam 21 abuts with the inlet valve 14 can be set by the separate rocker arms due to the primary and secondary rocker arms 50, 60 abutting with the inlet cam 21 and the 25 inlet valve 14, respectively, and since the primary and

secondary oscillating center lines L4, L5 oscillate together with the holder 30, even in case the shift amount of the primary rocker arm 50 is increased by virtue of the oscillation of the holder 30 in order to

5 set the control range of the valve operating properties large, when compared with the case where while one of the primary and secondary oscillating center lines shifts, the other does not, the relative shift amount of the primary and secondary rocker arms 50, 60 can be suppressed to a

10 small amount. As a result, the degree of freedom in arrangement of the transmission mechanism Mi is increased, and the application range thereof is expanded, and moreover, since the relative shift amount of the primary and secondary rocker arms 50, 60 can be suppressed to a small amount, the control range of the

15 valve operating properties can be set large.

As the oscillating position of the holder 30 approaches the primary limit position where the maximum valve operating property K_a can be obtained, the cam abutment position P1 between the cam abutment portion 52 and the cam lobe portion 21b approaches the specific straight line L10 on the orthogonal plane which intersects at right angles with the holder oscillating center line L3, whereby when the cam abutment position P1

20 is situated on the specific straight line L10, since the

25

line of action of the valve drive force is positioned on
the specific straight line L10, the moment generated
around the holder oscillating center line L3 to act on
the holder 30 based on the valve drive force acting via
5 the primary rocker arm 50 becomes zero. From this fact,
while since the maximum lift amount is increased as the
holder 30 approaches the primary limit position where the
valve operating property can be obtained where the
maximum lift amount of the inlet valve 14 becomes
10 maximum, the valve drive force is also increased, the
moment acting on the holder 30 can be reduced by allowing
the cam abutment position P1 on the cam lobe portion 21b
to approach the specific straight line L10, and the drive
force of the electric motor 28 which oscillates the
15 holder 30 against the moment, whereby the electric motor
28 is made compact.

The valve abutment portion 64 abuts with the valve
stem 14a of the inlet valve 14, and the holder
oscillating center line L3 is disposed on the extension
20 of the valve stem 14a which extends along the axis L7 of
the valve stem 14a, whereby the distance between the
holder oscillating center line L3 and the line of action
of the reaction force F2 from the inlet valve 14 is
maintained small within the range of the valve stem 14a,
25 and therefore, the moment acting on the holder 30 can be

reduced based on the reaction force F2, and in this respect, too, the embodiment can contribute to the reduction in driving force of the electric motor 28.

Next, referring to Fig. 9, a second embodiment of 5 the invention will be described below. The second embodiment differs from the first embodiment mainly as to a primary rocker arm 50 and a holder oscillating center line, and the former is constructed basically the same as the latter as to the other features, and therefore, while 10 the description of the same features will be omitted or briefly made, the description will be made as to different features of the second embodiment. Note that like reference numerals are given to members, as required, which are like or correspond to those described 15 in the first embodiment.

In the second embodiment, a roller 53 is disposed such that an cam abutment portion 52 of a primary rocker arm 50 may be positioned on a specific straight line 10 where a cam abutment position P1 passes through a holder oscillating center line L3 and a rotational center line 20 L2 on an orthogonal plane.

To be specific, as shown in Fig. 9, when a holder 30 occupies a primary limit position, the cam abutment position P1 situated on an apex 21b1 of a cam lobe 25 portion 21b is situated on the specific straight line

L10. Therefore, the roller 53 is disposed such that as the oscillating position of the holder 30 approaches a predetermined position where a maximum valve operating property can be obtained where a maximum lift amount of 5 an inlet valve 14 becomes maximum, the cam abutment position P1 residing at the apex 21b1 approaches the specific straight line L10.

Then, since when the cam abutment position P1 residing at the apex 21b1 is situated on the specific 10 straight line L10, the line of action of a valve drive force F1 is situated on the specific straight line L10, a moment generated around the holder oscillating center line L3 to act on the holder 30 based on the valve drive force F1 becomes zero.

According to the second embodiment, similar 15 functions and advantages to those in the first embodiment are provided, except for the fact that the valve operating properties are different, and in addition to the similar functions and advantages, the following 20 function and advantage will also be provided.

By adopting the construction in which in a primary rocker arm, a cam abutment position 52 is disposed such that when the holder occupies the primary limit position, the cam abutment position P1 may be situated on the 25 specific straight line L10, since when the cam abutment

position P1 is situated on the specific straight line L10, the line of action of the valve drive force F1 is situated on the specific straight line L10, the moment generated around the holder oscillating center line L3 to 5 act on the holder 30 based on the valve drive force F1 which acts via the primary rocker arm 50 becomes zero. Due to this, in the state where the cam abutment position P1 on the cam lobe portion 21b is situated on the specific straight line L10 and in the vicinity thereof, 10 since the drive force of an electric motor 28 which causes the holder 30 to oscillate against the moment can be reduced, the electric motor 28 is made compact.

Then, by adopting the construction in which the cam abutment position P1 is situated on the specific straight line L10 when the cam abutment position P1 resides at the apex 21b1 of the cam lobe portion 21b, since the moment acting on the holder 30 based on the maximum valve drive force F1 becomes zero at the specific oscillating position of the holder 30, the drive force of the 20 electric motor 28 can be reduced further.

As to embodiments in which part of the constructions of the embodiments that have been described heretofore are changed, the changed constructions will be described below.

25 Instead of the inlet operation mechanism, the

exhaust operation mechanism may be made up of the variable property mechanism, and both the inlet operation mechanism and the exhaust operation mechanism may be made up of the variable property mechanism. In addition, the 5 valve train may be such as to include a pair of camshafts including, in turn, an inlet camshaft on which an inlet cam is provided and an exhaust camshaft on which an exhaust cam is provided. In the aforesaid embodiments, while the primary member which regulates the oscillating 10 position of the secondary rocker arm 60 relative to the holder 30 is the primary oscillating member (the primary rocker arm 50) which is the oscillating member, the primary member may be a member which performs other movements than oscillation.

15 In stead of being formed on the drive abutment 54 of the primary rocker arm 50, the cam profile may be formed on the follower abutment portion 62 of the secondary rocker arm 60, and as this occurs, the portion, for example, a roller of the drive abutment portion of the 20 primary rocker arm 50 is brought into abutment with the cam profile. The abutment surface such as the cam abutment portion or the follower abutment portion 62 may be made up of other sliding surfaces, whose sectional shape is something like an arc, than the roller. The 25 primary and secondary rocker arms may be such as of a

swing type. In addition, in the secondary rocker arm 60, the valve abutment portion having the valve abutment surface may be such as to have no adjustment screw.

The drive mechanism Md may be such as to include,
5 instead of the drive gear 29b, a member or a link mechanism which is caused to oscillate by the drive shaft 29. In addition, the drive mechanism Md may be such as not to have the common drive shaft to all the cylinders and may be such as to have a drive shaft that is driven
10 by a separate actuator for a specific cylinder. By adopting this construction, the operation of part of the cylinders can be brought to rest in accordance with the operating conditions.

The holder oscillating center line L3 may be set at
15 a position where the center line L3 intersects at right angles with the axis L7 of the valve stem 14a. In addition, the position of the holder oscillating center line L3 may be set such that the reaction force F2 from the inlet valve 14 generates a moment acting in a
20 direction in which the moment based on the valve drive force F1 is cancelled thereby.

While the minimum valve operating property Kb is such that the maximum lift amount becomes zero, the minimum valve operating property Kb may be a valve
25 operating property where the maximum lift amount has a

value other than zero.

The inlet cam 14 relative to the crankshaft or a variable phase mechanism which can change the phase of the camshaft 20 may be provided on the camshaft 20 or the 5 valve transmission mechanism.

The holder 30 does not have to be made up of a separate member for each cylinder so as to be separate from one another but may be such that separate members are connected together by a connecting means or the 10 holder 30 may be formed integrally for all the cylinders.

When the cam abutment position P1 is situated at the base circle portion 21a, by adopting the construction in which the cam abutment portion is disposed such that the cam abutment position P1 is situated on the specific 15 straight line L10, a valve operating property can be obtained which has longer valve opening period and larger maximum valve properties than the valve operating properties obtained by the first embodiment.

In addition, while, in the second embodiment, in the 20 state where the holder 30 is situated at the primary limit position, when the cam abutment position resides at the apex of the cam lobe portion, the cam abutment portion is disposed such that the cam abutment position 25 is situated on the specific straight line, in a state where the holder is situated at any other oscillating

positions than the primary limit position, the cam
abutment portion may be disposed such that the cam
abutment position situated at the apex of the cam lobe
portion is positioned on the specific straight line or
5 the cam abutment position situated at any other locations
on the cam lobe portion than the apex is situated on the
specific straight line.

The internal combustion engine may be a single-
cylinder one and may be applied to equipment other than
10 vehicles, for example, to a marine propelling apparatus
such as outboard engines having a crankshaft which is
directed in a perpendicular direction.

While there has been described in connection with
the preferred embodiments of the present invention, it
15 will be obvious to those skilled in the art that various
changes and modification may be made therein without
departing from the present invention, and it is aimed,
therefore, to cover in the appended claim all such
changes and modifications as fall within the true spirit
20 and scope of the present invention.